

Impact of measurement uncertainty on building modeling and retrofitting decisions - Appendix

1 Appendix A. Heating system efficiency and sizing

For heat pumps, we consider seasonal performance factors for space heating (SPF_h) and DHW (SPF_{DHW}).

1.1 Appendix A.1. Air-to-water heat pumps

The bin-method was used from the Swiss standard SIA 384/3 (Swiss Society of Engineers and Architects (SIA), 2013) for the determination of the seasonal performance factors of heat pumps, as seen in Eq. 1.

$$COP(t) = a_0 + a_1 \cdot T_{source}(t) + a_2 \cdot T_{supply}(t) + a_3 \cdot T_{source}(t) \cdot T_{supply}(t) + a_4 \cdot T_{source}(t)^2 + a_5 \cdot T_{supply}(t)^2 \quad \text{Eq. 1}$$

For air-to-water heat pumps, the external temperature $T_e(t)$ is used as $T_{source}(t)$ in Eq. 1.

The hourly electricity demand for space heating is calculated by dividing the hourly space heating load $\Phi_H(t)$ by the coefficient of performance at the same time $COP(t)$ and multiplying by one hour for the conversion from power to energy as seen in Eq. 2.

$$E_h(t) = \frac{\Phi_h(t) \cdot 1h}{COP(t)} \quad \text{Eq. 2}$$

Then the seasonal coefficient of performance follows from Eq. 3.

$$SCOP_h = \frac{\sum_{t=1}^{8760} \Phi_h(t) \cdot 1h}{\sum_{t=1}^{8760} E_h(t)} \quad \text{Eq. 3}$$

In Eq. 3, $\Phi_H(t)$ is the hourly space heating load, and $E_h(t)$ is the hourly electricity demand for space heating.

The electricity demand for the circulation pump $E_{add,h}$ is calculated by multiplying the time of operation of the pump with the power of the circulation pump as seen in Eq. 4.

Eq. 4

$$E_{add,h} = t_{pump,h} \cdot P_{pump}$$

The seasonal performance factor for space heating SPF_h is then calculated with Eq. 5.

Eq. 5

$$SPF_h = \frac{\eta_{hp}}{\frac{1}{SCOP_h} + \frac{E_{add,h}}{Q_h}}$$

In Eq. 5, η_{hp} is the efficiency of the heat pump considering losses due to on-off cycling and Q_h is the yearly space heating demand of the building.

Due to the assumption of constant DHW supply temperature (T_{DHW}) and demand, the seasonal coefficient of performance for DHW can be calculated using Eq. 6.

Eq. 6

$$SCOP_{DHW}(t) = a_0 + a_1 \cdot T_{source,avg}(t) + a_2 \cdot T_{DHW}(t) + a_3 \cdot T_{source,avg}(t) \cdot T_{DHW}(t) + a_4 \cdot T_{source,avg}(t)^2 + a_5 \cdot T_{DHW}(t)^2$$

In Eq. 6, $T_{source,avg}$ is the yearly average outdoor air temperature that serves for air-to-water heat pumps. The calculation of $T_{source,avg}$ for geothermal heat pumps is available in Appendix A.

Auxiliary energy for DHW generation includes the energy for the circulation pump P_{pump} , and for the weekly heating of the DHW storage to 60°C for thermal disinfection as seen in Eq. 7.

Eq. 7

$$E_{add,DHW} = t_{pump,DHW} \cdot P_{pump} + 52 \cdot V_{DHW,storage} \cdot (60^\circ C - T_{DHW}) \cdot c_{p,water} \cdot \rho_{water}$$

In Eq. 7, $V_{DHW,storage}$ is the volume of the DHW storage tank.

The seasonal performance factor for DHW is calculated in Eq. 8.

Eq. 8

$$SPF_{DHW} = \frac{\eta_{hp}}{\frac{1}{SCOP_{DHW}} + \frac{E_{add,DHW}}{Q_{dhw}}}$$

In Eq. 8, η_{hp} considers losses of the buffer storage. The final energy for space heating and domestic hot water ($FED_{h\&DHW}$) is calculated as in Eq. 9.

$$FED_{h\&DHW} = \frac{Q_h}{SPF_h} + \frac{\frac{Q_{DHW}}{\eta_{DHW}}}{SPF_{DHW}} \quad \text{Eq. 9}$$

1.2 Appendix A.2. Ground source heat pump

For geothermal heat pumps, the $T_{source,avg}$ in Eq. 10 is the source temperature of the geothermal probe T_{source} . It is assumed to be constant and calculated according to (Swiss Society of Engineers and Architects (SIA), 2013; Huber and Stalder, 2020):

$$T_{source} = 10^\circ C - \left(0.005 \frac{^\circ C m}{W} + \frac{t_{op}}{100h} \cdot 0.006 \frac{^\circ C m}{W} \right) \cdot \Phi_{h,max} \cdot \frac{\frac{1000W}{kW}}{L_{probe}} \cdot \frac{COP_{B0/W35}-1}{COP_{B0/W35}} \quad \text{Eq. 10}$$

where $COP_{B0/W35}$ is the COP at $T_{source} = 0^\circ C$ and $T_{supply} = 35^\circ C$. t_{op} [h] is the total operating time of the heat and calculated as

$$t_{op} = \frac{Q_h + Q_{DHW}}{\Phi_{h,max}} \quad \text{Eq. 11}$$

2 Appendix B. Design parameters

Table 2.1: List of design parameters chosen for the building energy assessment, cost assessment, and environmental assessment

Variable	Value	Source
$T_{i,design}$	20 °C	SIA 380/1 (Swiss Society of Engineers and Architects (SIA), 2016)
$T_{e,design}$	-9 °C	SIA 2028 (Swiss Society of Engineers and Architects (SIA), 2010)
T_{limit}	15 °C	Assumption based on oil boiler setting in case study building
ΔT	8 °C	Assumption
$V_{DHW,storage}$	0.3 m ³ /d	DHW storage in case study building
P_{pump}	50 W	Manual of pump in case study building
$t_{pump,h}$	2300 h	Handbook (Swiss Federal Office of Energy, 2019)
$t_{pump,DHW}$	400 h	Handbook (Swiss Federal Office of Energy, 2019)
$\eta_{h,geo}$	SPF_h, SPF_{DHW}	Appendix A
$\eta_{h,air}$	SPF_h, SPF_{DHW}	Appendix A
$\eta_{h,district}$	0.97	SIA 380/1 (Swiss Society of Engineers and Architects (SIA), 2016)
$\eta_{h,wood}$	0.75	SIA 380/1 (Swiss Society of Engineers and Architects (SIA), 2016)
η_{hp}	0.96	SIA 380/1 (Swiss Society of Engineers and Architects (SIA), 2016)
η_{DHW}	0.8	SIA 380/1 (Swiss Society of Engineers and Architects (SIA), 2016)
P_{Wood}	0.08 CHF/kWh	IEA EBC Annex 56 (Ott et al., 2017)
$P_{District\ heat}$	0.09 CHF/kWh	IEA EBC Annex 56 (Ott et al., 2017)
$P_{Electricity}$	0.21 CHF/kWh	IEA EBC Annex 56 (Ott et al., 2017)
$CF_{GHG,Wood}$	0.027 kg-CO ₂ /kWh	KBOB 2016 (Bächtold et al., 2016)
$CF_{GHG,District}$	0.108 kg-CO ₂ /kWh	KBOB 2016 (Bächtold et al., 2016)
$CF_{GHG,Electricity}$	0.102 kg-CO ₂ /kWh	KBOB 2016 (Bächtold et al., 2016)
IC_{Wood}	97 CHF/kW	Quotation (Sigrist et al., 2019)
$IC_{District}$	128 CHF/kW	Quotation (Sigrist et al., 2019)
IC_{air}	648 CHF/kW	Quotation (Sigrist et al., 2019)
IC_{geo}	2122 CHF/kW	Quotation (Sigrist et al., 2019)
r_{ec}	0%	Assumption
r	0%	Assumption
τ	30 years	Assumption

3 References

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