

## Supplementary Material

## High Anodic-Voltage Focusing of Charge Carriers in Silicon Enables the Etching of Regularly-Arranged Submicrometer Pores at High Density and High Aspect-Ratio

### Chiara Cozzi<sup>1†</sup>, Giovanni Polito<sup>1†</sup>, Lucanos M. Strambini<sup>2</sup>, Giuseppe Barillaro<sup>1,2\*</sup>

<sup>1</sup>Dipartimento di Ingegneria dell'Informazione, Università di Pisa, via G. Caruso 16, 56122 Pisa, Italy

<sup>2</sup>Istituto di Elettronica e di Ingegneria dell'Informazione e delle Telecomunicazioni, Consiglio Nazionale delle Ricerche, via G. Caruso 16, 56122, Pisa, Italy

<sup>†</sup>These authors contributed equally to this work.

\* Correspondence: Corresponding Author: g.barillaro@iet.unipi.it

#### **1** Supplementary Data

#### 1.1 Electrochemical etching setup

The electrochemical etching setup includes a three-electrode polytetrafluorethylene (PTFE) electrochemical etch-cell with a volume of 400 cm<sup>3</sup>. The front-side of the silicon electrode is in contact with the electrolyte through a circular-shaped aperture identifying an etching area (E<sub>A</sub>) of  $\sim 0.64$  cm<sup>2</sup>. A halogen lamp (250 W) positioned 5 cm away from the silicon electrode is used to photogenerate a hole current by illuminating the silicon back-side through a circular window (1.3 cm<sup>2</sup>) in the metal electrode providing the electrical contact to the sample itself. The photogenerated hole current was properly controlled as the etching progressed changing the lamp power and, in turn, the illumination intensity by means of a feedback loop performed using a proportional-integralderivative (PID) controller (Eurotherm 2604). An IR filter with a cut-off wavelength of 750 nm was placed between the lamp and the silicon sample to avoid charge carrier generation close to the silicon surface in contact with the electrolyte, whereas the electrolyte was stirred during the etching to enhance the etching uniformity. The working temperature was kept constant at 22 °C for the entire etching time through a second feedback loop implemented using another PID controller. A platinum disk placed at 1 cm from the silicon anode and a platinum wire placed at about 2 mm from the silicon electrode were used as cathode and pseudo-reference electrodes immersed in the HF-aqueous electrolyte, respectively. A Source Measure Unit (Keithley 2410 Source Meter) was used to apply the anodization voltage between the silicon slab and the reference electrode, and to monitor the photogenerated current.

# **1.2** Electrolyte/silicon interface radius of curvature and anodic voltage effects on the the depletion region establishing at the pore tip

Assuming that the pore tip has a spherical surface with curvature radius  $r_v$  varying from  $r_{min}$  at the apex to  $r_{max}$  at the pore base, it is feasible to solve the Poisson equation at the electrolyte/silicon interface:

$$\frac{1}{r^2}\frac{d}{dr}[r^2E(r)] = \frac{\rho(r)}{\varepsilon}$$
(S1)

being *r* the distance from center of the spherical surface,  $\varepsilon$  the dielectric constant of silicon, E(r) the electric field, and  $\rho(r)$  the charge density. Figure 2b shows a cross-section of the pore tip spherical surface with curvature radius  $r_o$ , also highlighting the depletion region  $w_a$  established within the silicon electrode. The charge density  $\rho(r)$  into the silicon volume is  $-qN_o$  for  $r_o \le r \le r_o + w_a$  and zero elsewhere, being  $N_o$  the ionized donor density, q the elementary electron charge, and  $w_a$  the width of the depletion region. By solving equation S1 for silicon using fully-depletion approximation (i.e. boundary conditions for electric field  $E(r_o + w_a) = 0$  V/m and potential  $V(r_o + w_a) = 0$  V (Muller and Kamins, 1977)), the following relationships between E(r), V(r), and  $r_o$  are obtained:

$$E(r) = \frac{qN_D}{3\varepsilon_s} \left[ -r + \frac{(r_0 + w_d)^3}{r^2} \right]$$
(S2)

$$V(r) = \frac{q_{N_D}}{6\varepsilon_s} \left[ r^2 + \frac{2(r_0 + w_d)^3}{r} - 3(r_0 + w_d)^2 \right]$$
(S3)

being  $\varepsilon_a = 1.05365 \times 10^{40}$  F/m the silicon dielectric constant. For a given potential difference  $V_a$  applied across the electrolyte/silicon interface, it is possible to obtain a relationship between the depletion region width  $w_a$  within the silicon electrode and  $V_a$  by assuming  $V(r_a) = -V_a$  in the equation S3:

$$V(r_0) = \frac{q_{N_D}}{6\varepsilon_s} \left[ r_0^2 + \frac{2(r_0 + w_d)^3}{r_0} - 3(r_0 + w_d)^2 \right] = -V_d$$
(S4)

$$w_d^3 + \frac{3}{2}r_0w_d^2 + \frac{6\varepsilon_s V_d}{qN_D} = 0$$
 (S5)

The width  $w_a$  of the depletion region into the silicon electrode is the solution of equation S5, given by solving a third order equation with real numbers coefficients as follow:

$$w_d^3 + aw_d^2 + bw_d + c = 0 (S6)$$

Being:

$$a = \frac{3}{2}r_0$$
,  $b = 0$ ,  $c = \frac{6\varepsilon_s V_d}{qN_D}$ 

Assuming:

$$P = -\frac{a^2}{9} = -\frac{r_0^2}{4} , \quad Q = \frac{-2a^3 + 9ab - 27c}{54} = -\frac{1}{8} \left( r_0^3 + 12 \frac{\varepsilon_s V_d}{qN_D} r_0 \right)$$

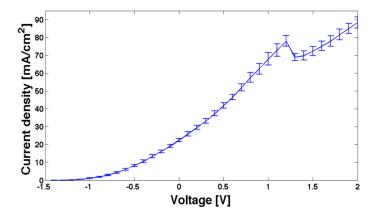
$$D = P^{3} + Q^{2} = \frac{3}{16} \frac{\varepsilon_{s} V_{d}}{q N_{D}} r_{0}^{2} \left( 2r_{0}^{2} + 4 \frac{\varepsilon_{s} V_{d}}{q N_{D}} \right)$$

Being *D* a positive number, equation S6 has only one real solution that can be figure out as follow:

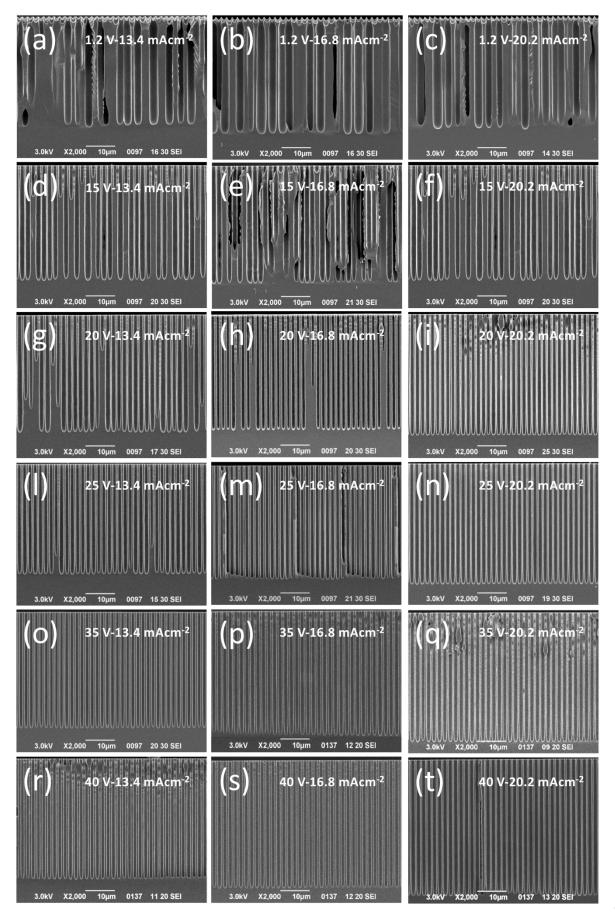
$$R = \sqrt[3]{Q + \sqrt{D}}, \quad S = \sqrt[3]{Q - \sqrt{D}}$$
$$w_d = -\frac{a}{3} + R + S = -\frac{r_0}{2} + R + S$$
(S7)

Expression S7 relates the width  $w_a$  of the depletion region into the silicon substrate to the potential difference  $V_a$  and to the radius of curvature  $r_a$  for a spherical shaped electrolyte/silicon interface. An increase of the electrolyte/silicon interface radius of curvature  $r_a$  and/or the potential difference  $V_a$  leads to an increase of the depletion region width  $w_a$ . For these reasons, the depletion region width for the actual pore tip reaches a minimum at the apex. An increase of the electrolyte/silicon interface radius of curvature  $r_a$  leads to a decrease of the maximum value assumed by the electric field into the silicon substrate. with a significant reduction of  $E_{max}$  only in the first 100 nm (of about one order of magnitude for  $r_a$  moving from 10 nm to 100 nm). On the contrary, an increase of the potential difference  $V_a$  leads to an increase of  $E_{max}$ , with a variation of about one order of magnitude moving from the low-voltage to the high-voltage anodic regime. As shown by the simplified model implemented, the actual pore tip is the electrolyte/silicon interface region where the electric field is highest, and its value can be noteworthy increased by increasing the anodic voltage.

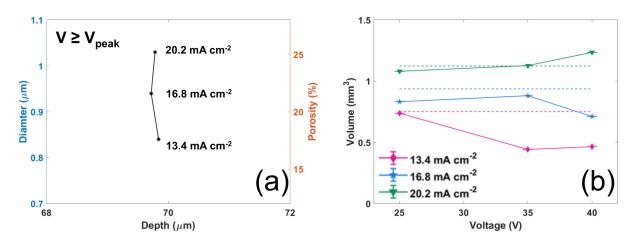
#### 2 Supplementary Figures and Tables



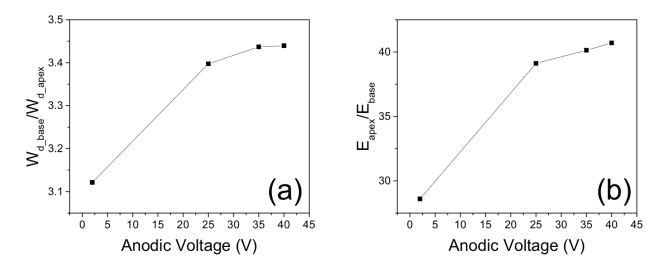
**Figure S1.** Electrochemical characterization of silicon dissolution in HF-based electrolyte solution by linear sweep voltammetry. Experimental current density-voltage curve (average value and standard deviation) of n-type silicon electrode in the presence of HF concentration of 5 vol% under back-side higher-intensity illumination (100% of the 250 W halogen lamp power).



**Figure S2.** Influence of the etching voltage  $V_{ext}$  and the etching current density  $J_{ext0}$  value on the controlled etching of pores with sub-micrometric diameter and spacing below 2 µm. Cross section SEM images showing (a-c) the uncontrolled etching resulting by performing the BIEE with  $V_{ext0}=1.2$  V and (a)  $J_{act0}=13.4$  mA cm<sup>2</sup>, (b)  $J_{act0}=16.8$  mA cm<sup>2</sup>, and (c)  $J_{ext0}=20.2$  mA cm<sup>2</sup>; (d-i) the uniform pore nucleation resulting from the beneficial effect of the increased etching voltage to (d-f)  $V_{act0}=15$  V, and (g-i) with  $V_{act0}=20.2$  mA cm<sup>2</sup>; (e,h)  $J_{ect0}=16.8$  mA cm<sup>2</sup>, and (f,i)  $J_{ext0}=20.2$  mA cm<sup>2</sup> leading to pore formation in all available defect sites in silicon samples etched by BIEE, showing only a limited number of shorter pores; (l-t) the uniform array of ordered pores featuring same depth and diameter successfully obtained by BIEE performed at (l-n)  $V_{ect0}=25$  V, (o-q)  $V_{ext}=35$  V, and (r-t) with  $V_{ect0}=40$  V with (l,o,r)  $J_{ext0}=13.4$  mA cm<sup>2</sup>, (m,p,s)  $J_{ext0}=16.8$  mA cm<sup>2</sup>, and (n,q,t)  $J_{ext0}=20.2$  mA cm<sup>2</sup>.



**Figure S3.** (a) Expected pore diameters (left axis) with corresponding expected porosities (right axis) as a function of expected pore depths corresponding to each of the  $J_{ect0}$  values investigated. (b) Calculated (solid lines) and theoretical (dashed lines) volume of dissolved silicon as a function of anodic voltages for each of the  $J_{ect0}$  values investigated.



**Figure S4.** (a) Theoretical ratio between width of the depletion region at the pore base (i.e. curvature radius 500 nm) and tip apex (i.e. curvature radius 100 nm); (b) Theoretical ratio between maximum electric field intensity at the tip apex (i.e. curvature radius 100 nm) and pore base (i.e. curvature radius 500 nm).

Anodization Voltage	Etching Current Density		Expected Porosity	Expected Diameter
$V_{\text{etch}}\left[V ight]$	Starting value $J_{etch0}$ [mA cm <sup>-2</sup> ]	Slope α [μA s <sup>-1</sup> cm <sup>2</sup> ]	P. [%]	d₊ [µm]
	13.4	-0.938	17.2	0.842
1.2, 15, 20, 25, 35, 40	16.8	-1.219	21.5	0.942
	20.2	-1.453	25.8	1.032

**Table S1:** Parameters (i.e. anodic voltage and etching current density) used in this work for the electrochemical etching of silicon substrates with resistivity of 3-8  $\Omega$  cm pre-patterned with lattice of square holes with side of 1  $\mu$ m and spacing of 1.8  $\mu$ m, and values expected (i.e. porosity and diameter of pores).